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A Comparison of Landslide Susceptibility Maps Produced by Weighted Linear Combination and Analytical Hierarchy Process Methods: A Case Study at Khao Phanom Bencha Watershed in Krabi Province

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Abstract

This study compared the abilities of the Weighted Linear Combination (WLC) and Analytical Hierarchy Process (AHP) methods in producing credible landslide susceptibility maps for the study area at Khao Phanom Bencha Watershed in Krabi Province, southern Thailand. A reference landslide inventory was established from identified landslide events appearing on 4 sources of high-resolution satellite imagery (THEOS, EO-1, Google Earth, and Bing Map). Ten crucial contributing factors were incorporated in the susceptibility analysis in both methods, i.e., elevation, slope gradient, slope aspect, slope curvature, Topographic Wetness Index (TWI), distance from drainage, distance from lineament, lithology, soil texture, and land use/land cover (LULC). All yielded susceptibility maps were assessed for their respective accuracies in predicting the referred landslide incidences (290 samples in total), based on 2 well-known methods: the Area-Under-Curve (AUC) and the Receiver Operating Characteristic (ROC) analysis. Average accuracies of the maps achieved by the WLC and AHP methods were found to be significantly high, at 85.81 and 82.42 %, respectively. These maps are useful for the preparation of effective strategic planning for the prevention and mitigation of landslide hazards in the area by responsible agencies and local authorities.

Keywords: Landslide susceptibility map, Weighted Linear Combination (WLC), Analytical Hierarchy Process (AHP), Area-Under-Curve (AUC), Receiver Operating Characteristic (ROC)

Introduction

Landslides are well-known natural phenomena involving a mass movement of soil (in the forms of earth or debris) or rock downward along a slope under gravitational influence [1,2]. At present, landslides are regarded as one of the most destructive of hazards, which induces a substantial loss of life and vast damage to property and the natural environment worldwide [3-5]. Therefore, prior knowledge of the areas prone to destructive landslides is highly essential for most countries, especially those in the tropics or in the earthquake dominated zone, to help with preparing proper strategies for the prevention or mitigation of the potential landslide risk. Conventionally, a detailed map illustrating the distribution of these landslide-prone areas is called a landslide susceptibility map.

In principle, there are 2 broad groups of landslide susceptibility evaluating methods; the qualitative (or heuristic) type, and the quantitative type. For the qualitative approach, the final decision on landslide potential over an area is determined based mainly on collective expert opinions (on the nature of landslide characteristics experienced within an area). This concept was widely used as a basic methodology for the construction of initial landslide susceptibility zoning by landslide researchers for a long time. However, in recent decades, more complicated methods of the quantitative type, which make decisions on this issue http://wjst.wu.ac.th

based on information on past landslide events that have taken place in the area, were introduced to build more realistic susceptibility maps for an area; these methods include the frequency ratio (FR) or Multiple Logistic Regression (MLR) methods, e.g., in [6-9].

Attention paid to the identification of landslide prone areas (or susceptibility analysis) and the assessment of the potential impacts on humans and the environment (risk analysis) has risen dramatically in recent decades, due to mounting public concern on these issues. As validity of a gained landslide susceptibility map depends principally on the used methods and their input data, comparative studies to evaluate the efficiency of several recommended methods in the preparation of landslide susceptibility maps for an area of interest has been reported more often in recent years, such as [5,10-14]. The main objectives of these studies were to identify the capability of the tested methods in generating a highaccuracy landslide susceptibility map for the preferred area, from which the most effective procedure can then be applied in subsequent hazard and risk analysis.

For this work, the capability of 2 popular qualitative methods; the Weighted Linear Combination (WLC) and Analytical Hierarchy Process (AHP), was evaluated and compared for the study area of Khao Phanom Bencha Watershed in Krabi Province, southern Thailand. This place was chosen due primarily to its status as one of the landslide hotspots in Thailand, where devastating landslide incidences were reported several times in recent decades. The referred area is located on the Andaman Coast of southern Thailand, covering land of about 987.53 km^2 and dominated by mountainous topography (Figure 1). The watershed has a central mountain network that aligns along the north-south direction, approximately, as its outstanding landmark. Frequent landslide activities occur as a result of the rough mountainous landscape and a fairly high amount of annual rainfall [15]. However, rapid changes in land use patterns in the area, due to continuous conversion of the forest lands into several kinds of economic agricultural plantations (e.g., para rubber and oil palm) and communities into the known landslide-prone locations, have recently become a cause for high public concern. This is because forest clearance for expansive plantations of the shallow-rooted crops, orchards, or trees, might enable more massive landslide incidence, with higher losses of human lives or higher amount of gross damages to important infrastructures and the natural environment [16,17].



Figure 1 Location map of the study area, Khao Phanom Bencha Watershed in Krabi Province.

Materials and methods

Materials

The required input data were acquired from responsible agencies and from other relevant resources (as detailed in **Table 1**) and then restructured to have the proper format for further use (in the form of a GIS-based dataset). Ten typical causative factors of landslide activity in tropical zones were included in the construction of the preferred susceptibility map: elevation, slope gradient, slope aspect, slope curvature, Topographic Wetness Index (TWI), distance from drainage, distance from lineament, lithology, soil texture, and Land Use/Land Cover (LULC) (**Figures 2(a) - (j)**). These factors can be grouped into 3 broad categories: geological, topographical and environmental types.

Table 1 List of necessary input data and their respective sources.

| Classification | | | GIS | Scale or | Original | Note |
|---------------------|-----------------|---------|------------|------------|----------|-------------|
| Data category | Details | | data type | resolution | sources | Note |
| Land use/Land cover | LULC-2009 | | Polygon | 1:25,000 | LDD | Figure 2(j) |
| | Elevation | | | | | Figure 2(a) |
| | Slope gradient | | | | | Figure 2(b) |
| Topography | Slope aspect | | | | | Figure 2(c) |
| | Slope curvature | \prec | Point/Line | 1:50,000 | RTSD | Figure 2(d) |
| Landform | TWI | | | | | Figure 2(e) |
| Stream | Stream network | | | | | Figure 2(f) |
| Castan | Lithology | ~ | Polygon | 1:250,000 | DMR | Figure 2(h) |
| Geology | Lineament | | Line | 1:250,000 | DMR | Figure 2(g) |
| Soil | Soil texture | | Polygon | 1:100,000 | LDD | Figure 2(i) |

Note: $DMR \equiv Department of Mineral Resources; LDD \equiv Land Development Department; RTSD = Royal Thai Survey Department.$

Methods

Construction of landslide inventory map

The landslide inventory map was formulated based on accumulated data of past landslide occurrences within the area, mainly from devastating incidences reported in March 2011. These data were visually extracted from distinctive landslide scars found in high-resolution satellite imagery, like those from the THEOS (or Thaichote) satellite recorded on 15th April 2011 (at a spatial resolution of 2.0 m) or NASA's EO-1 satellite taken on 4th April 2011 (at a spatial resolution of 10 m). Also, distributed satellite imagery recorded over the area around that time (with landslide traces evidenced), found on the Google Earth and Bing Map websites, were also incorporated into the analysis. **Figure 3** demonstrates compared examples of several distinctive landslide scars on the used satellite imagery assembled from those 4 listed sources. Only cloud-free images were employed for this task. Eventually, a total of 210 identified landslide samples were applied for the accuracy assessment procedure of all yielded susceptibility maps.

Construction of the landslide susceptibility map

This part consists of 2 principal tasks. The first one is to formulate the landslide susceptibility maps for the area. The second task is to assess the accuracy of the resulting maps gained from each applied method. A flowchart of the main work in this part is shown in **Figure 4**. The appropriate weights of the factor and attribute (or class) level of both methods were determined from the independent judgments of 8 associated experts in this field, collected through the distributed questionnaires for each method. The net contributing weight [= Factor Weight (FW) × Class Weight (CW)], or NCW, for each attribute of a evaluated factor was then assessed (for each method) and used as a basis for the generation of the landslide susceptibility score (LSS) and the normalized susceptibility score (NSS) for a specific pixel, as follows (for 10 contributing factors);

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Slope e (a) Elevation (b) Slope gradient (c) Slope aspect (d) Slope curvature (e) TWI (f) Distance from drainage (g) Distance from (h) Lithology lineament (j) LULC (i) Soil texture Figure 2 Landslide related factors in the study area.





(c) Google Earth

(d) Bing Map

Figure 3 Examples of the high-resolution satellite images from 4 different sources; (a) THEOS satellite, (b) EO-1 satellite, (c) Google Earth website, (d) Bing Map website, showing landslide traces over the study area (from the expansive landslide incidence in late March 2011).

$$LSS_{i} = \sum_{j=1}^{10} NCW_{i,j};$$
(1)

$$NSS_{i} = \frac{LSS_{i} - LSS_{min}}{LSS_{max} - LSS_{min}};$$
(2)

where LSS_i is the LSS value for pixel i^{th} on the map, and LSS_{max} and LSS_{min} are the maximum and minimum values of LSS found on the map, respectively.

NSI represents the relative probability of a landslide occurrence; therefore, the higher the index, the more susceptible the area is to landslide occurrence. If the NSI value is high, there is a higher susceptibility to landslides; a lower value indicates a lower susceptibility to landslides. These NSI values were divided into 5 classes, based on the equal interval classification method, to represent 5 different susceptibility zones on the resulting map, which are Very High Susceptibility (VHS), High Susceptibility (HS), Moderate Susceptibility (MS), Low Susceptibility (LS), and Very Low Susceptibility (VLS).

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Figure 4 Work flowchart for the construction and verification of the preferred landslide susceptibility maps.

Table 2 FW and class (or attribute) weights for each input data and their attributes for the WLC method in which the proposed range of both weight types is from 1 (least important) to 5 (most important).

| Thematic layers | Attributes | FW | CW | Net contributing weights (FW·CW) |
|-----------------|---------------------------|------|------|-------------------------------------|
| Elevation | < 200 m | 2.38 | 1.25 | 2.9750 |
| | 200 m – 400 m | | 2.13 | 5.0694 |
| | 400 m – 600 m | | 2.88 | 6.8544 |
| | 600 m – 800 m | | 3.88 | 9.2344 |
| | 800 m – 1,000 m | | 4.63 | 11.0194 |
| | > 1,000 m | | 4.50 | 10.7100 |
| Slope gradient | $0^{\circ} - 10^{\circ}$ | 4.50 | 1.00 | 4.5000 |
| | $10^{\circ} - 20^{\circ}$ | | 2.00 | 9.0000 |
| | $20^{\circ} - 30^{\circ}$ | | 3.00 | 13.5000 |
| | $30^{\circ} - 40^{\circ}$ | | 3.88 | 17.4600 |
| | $40^{\circ} - 50^{\circ}$ | | 4.13 | 18.5850 |
| | > 50° | | 4.38 | 19.7100 |

| Thematic layers | Attributes | FW | CW | Net contributing weight (FW·CW) |
|--------------------------|----------------------------|------|------|------------------------------------|
| Slope aspect | Flat | 2.38 | 1.00 | 2.3800 |
| | North | | 1.50 | 3.5700 |
| | Northeast | | 2.50 | 5.9500 |
| | East | | 2.88 | 6.8544 |
| | Southeast | | 2.50 | 5.9500 |
| | South | | 3.00 | 7.1400 |
| | Southwest | | 3.63 | 8.6394 |
| | West | | 3.63 | 8.6394 |
| | Northwest | | 2.25 | 5.3550 |
| Slope curvature | Concave (-) | 2.75 | 2.50 | 6.8750 |
| Stope eta tatale | Flat (0) | 2.70 | 1.38 | 3.7950 |
| | Convex (+) | | 3.50 | 9.6250 |
| TWI | 0 - 2.5 | 2.88 | 1.00 | 2.8800 |
| 1 W1 | 2.5 - 5.0 | 2.00 | 2.00 | 5.7600 |
| | 2.5 – 5.0 5.0 – 7.5 | | 3.00 | 8.6400 |
| | 7.5 - 10.0 | | 3.75 | 10.8000 |
| | | | 4.75 | |
| | 10.0 - 12.5 | | | 13.6800 |
| D | > 12.5 | 2 00 | 5.00 | 14.4000 |
| Drainage | < 50 m | 2.88 | 4.88 | 14.0544 |
| (Distance from drainage) | 50 m - 100 m | | 4.13 | 11.8944 |
| | 100 m – 150 m | | 3.25 | 9.3600 |
| | 150 m – 200 m | | 2.25 | 6.4800 |
| | 200 m – 250 m | | 1.38 | 3.9744 |
| | > 250 m | | 1.00 | 2.8800 |
| Lithology | Thung Yai | 4.29 | 3.14 | 13.4706 |
| | Ratburi | | 1.57 | 6.7353 |
| | Sediment | | 1.57 | 6.7353 |
| | Kaeng Krachan | | 3.71 | 15.9159 |
| | Igneous rocks | | 5.00 | 21.4500 |
| | Krabi | | 3.00 | 12.8700 |
| | Saibon Formation | | 3.00 | 12.8700 |
| Lineament | < 500 m | 3.00 | 5.00 | 15.0000 |
| (Distance from | 500 m – 1,000 m | | 4.13 | 12.3900 |
| lineament) | 1,000 m – 1,500 m | | 2.88 | 8.6400 |
|) | 1,500 m - 2,000 m | | 2.13 | 6.3900 |
| | 2,000 m - 2,500 m | | 1.63 | 4.8900 |
| | 2,500 m - 3,000 m | | 1.25 | 3.7500 |
| | > 3,000 m | | 1.13 | 3.3900 |
| | > 5,000 m | | 1.15 | 5.5900 |
| Soil Texture | Clay | 3.88 | 1.88 | 7.2944 |
| Son Texture | Silty clay | 5.00 | 2.13 | 8.2644 |
| | Loamy sand | | 3.25 | 12.6100 |
| | Sandy loam | | 3.13 | |
| | Sality clay loam | | 3.00 | 12.1444 11.6400 |
| | | | | |
| | Sand | | 3.25 | 12.6100 |
| | Sandy clay loam | | 3.13 | 12.1444 |
| | Clay loam | | 2.38 | 9.2344 |
| | Silty loam | | 2.63 | 10.2044 |
| | Loam | | 2.88 | 11.1744 |
| | Slope complex area | | 3.63 | 14.0844 |
| LULC | Dense evergreen forest | 3.00 | 1.38 | 4.1400 |
| | Disturbed evergreen forest | | 2.88 | 8.6400 |
| | Oil palm | | 3.50 | 10.5000 |
| | Para rubber | | 4.00 | 12.0000 |
| | Miscellaneous | | 3.50 | 10.5000 |

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Results and discussion

Weight quantification in the WLC method

From knowledge of the expert-based weighting data obtained in the WLC method (as reported in **Table 2**), it was obvious that, in terms of the priority, slope gradient, lithology, and soil texture were rated highest, with respective FW of 4.50, 4.29, and 3.88, while elevation, slope aspect, and slope curvature were scored lowest, with FW of 2.38, 2.38, and 2.75. At attribute level, the preferable conditions for landslide occurrence were high elevation (e.g. > 800 m), steep slope (e.g. > 40°), high TWI (e.g. > 10.0), relatively close distance to drainage (e.g. < 200 m) and the lineament (e.g. < 1,000 m), and igneous rock foundation. The most favorable aspects were found to be the southwest and west directions, with equal CW of 3.63. For the LULC aspect, para rubber planting was rated the most significant cause of landslide activity in the area (with CW of 4.00). The factor's order of priority (in terms of the factor weight) found in this work is rather similar to that presented in several WLC-based works reported earlier, especially on the favored top 2 candidates (slope gradient and lithology), e.g., in the works of [16,18,19]. For the attribute's merit (in terms of the attained class weight) of each of the listed factors, it often conforms well to conventional beliefs or prevalent theories. For examples, areas with higher slope gradients should be more susceptible to slope failure, as are those located closer to the drainage or lineament, or with igneous rock foundation. Areas situated in slope complex areas are also believed to most prone to landslide activity.

Weight quantification in the AHP method

The AHP method is also a very popular qualitative approach in decision-making analysis. However, in addition to the expert-based judgment on the value of the possible option, the consistency of this judgment by an individual expert is also examined. In this method, a pair-wise comparison matrix was established first from the comparative judgment of each corresponding expert, to attain a preference scale of these used factors (and the respective attributes), given in terms of a normalized weight between 0 and 1. In this case, the validity of each given judgment was determined, and those with a consistency ratio (CR) of < 0.10 were included in further analysis. **Tables 3** and 4 present the normalized weight outputs for all input factors and their respective set of attributes, while **Table 5** summarizes the yielded values of the Factor Weights and Class Weights (FW and CW) reported earlier in **Tables 3** and 4.

| Factors | | FW from individual expert judgment | | | | | | Mean weights | |
|--------------------|--------|------------------------------------|--------|--------|--------|--------|--------|-----------------|------------|
| (Input layer) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | (CR < 0.1) |
| Elevation | 0.0227 | 0.0735 | 0.0460 | 0.0551 | 0.0206 | 0.0181 | 0.0802 | 0.0200 | 0.0550 |
| Slope gradient | 0.2796 | 0.2431 | 0.2652 | 0.0468 | 0.2601 | 0.2807 | 0.2015 | 0.1101 | 0.1733 |
| Slope aspect | 0.0600 | 0.0171 | 0.0276 | 0.0776 | 0.1790 | 0.0194 | 0.0692 | 0.0671 | 0.0517 |
| Slope curvature | 0.0297 | 0.1179 | 0.0295 | 0.0806 | 0.1292 | 0.0346 | 0.0355 | 0.1127 | 0.0752 |
| TŴĪ | 0.0415 | 0.0332 | 0.0718 | 0.0692 | 0.0271 | 0.0933 | 0.0423 | 0.1807 | 0.0794 |
| Drainage | 0.1625 | 0.0170 | 0.0918 | 0.0702 | 0.0457 | 0.0626 | 0.0395 | 0.0540 | 0.0545 |
| Lithology | 0.1014 | 0.2511 | 0.1646 | 0.1663 | 0.1327 | 0.0986 | 0.0211 | 0.2750 | 0.1756 |
| Lineaments | 0.0675 | 0.1513 | 0.1815 | 0.0522 | 0.0413 | 0.0813 | 0.0478 | 0.0908 | 0.1047 |
| Soil texture | 0.1529 | 0.0588 | 0.1011 | 0.1481 | 0.1047 | 0.1498 | 0.2314 | 0.0526 | 0.1184 |
| LULC | 0.0820 | 0.0370 | 0.0211 | 0.2339 | 0.0595 | 0.1617 | 0.2314 | 0.0370 | 0.1121 |
| Consistency ratio: | 0.15 | 0.07 | 0.09 | 0.09 | 0.14 | 0.12 | -0.03 | 0.07 | |

Table 3 FW from pair-wise comparison matrix yielded from 8 experts.

Note: Only judgments with CR < 0.1 were used to calculate mean weight.

From the data shown in **Table 3**, slope gradient, lithology, and soil texture are still on top in terms of preference, like in the WLC method, with FW of 0.1733, 0.1756, and 0.1184, respectively, while the 3 lowest scores now belong to aspect, drainage, and elevation, with FW of 0.0517, 0.0545, and 0.0550,

respectively. At attribute level (based on data in **Table 4**), the favorite areas for landslide activity resemble those of the WLC method, e.g., those with relatively high elevation, steep slope, close distance to the lineament and drainage system, high TWI, or with igneous rock foundation. The 2 most preferred aspect choices are still the southwest and west; for LULC, these are oil palm and para rubber planting.

 Table 4 CW from pair-wise comparison matrix based on expert opinions.

| Factors | | CW (of each factor) from individual expert judgment | | | | | | Mean weight | |
|-------------------------------|--------|---|--------|--------|--------|--------|--------|----------------|------------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | (CR < 0.1) |
| Elevation (m) | | | | | | | | | |
| (1) < 200 | 0.0408 | 0.0260 | 0.0499 | 0.0469 | 0.0372 | 0.0434 | 0.0580 | 0.0268 | 0.0387 |
| (2) 200 - 400 | 0.0633 | 0.0471 | 0.1656 | 0.0677 | 0.0478 | 0.0655 | 0.0872 | 0.0498 | 0.0724 |
| (3) 400 - 600 | 0.1344 | 0.0886 | 0.1937 | 0.1132 | 0.0971 | 0.1024 | 0.1226 | 0.0864 | 0.1165 |
| (4) 600 - 800 | 0.4186 | 0.1660 | 0.3159 | 0.1132 | 0.1684 | 0.1604 | 0.1677 | 0.1824 | 0.2179 |
| (5) 800 - 1,000 | 0.1965 | 0.3362 | 0.1523 | 0.2140 | 0.2532 | 0.2488 | 0.2302 | 0.2077 | 0.2298 |
| (6) > 1,000 | 0.1464 | 0.3362 | 0.1225 | 0.4449 | 0.3962 | 0.3794 | 0.3344 | 0.4469 | 0.3246 |
| Consistency ratio: | 0.08 | 0.05 | 0.03 | 0.10 | 0.03 | 0.02 | 0.11 | 0.05 | |
| Slope gradient | | | | | | | | | |
| $(1) 0^{\circ} - 10^{\circ}$ | 0.0484 | 0.0269 | 0.0464 | 0.0458 | 0.0361 | 0.0309 | 0.0379 | 0.0301 | 0.0378 |
| (2) $10^{\circ} - 20^{\circ}$ | 0.0731 | 0.0488 | 0.1658 | 0.0712 | 0.0549 | 0.0428 | 0.0591 | 0.0567 | 0.0733 |
| $(3) 20^{\circ} - 30^{\circ}$ | 0.1868 | 0.1137 | 0.3998 | 0.1018 | 0.0767 | 0.0720 | 0.1001 | 0.0707 | 0.1459 |
| (4) $30^{\circ} - 40^{\circ}$ | 0.3730 | 0.1875 | 0.2452 | 0.1636 | 0.1397 | 0.1564 | 0.1562 | 0.1323 | 0.1997 |
| $(5) 40^{\circ} - 50^{\circ}$ | 0.1494 | 0.3116 | 0.0956 | 0.1636 | 0.2543 | 0.2759 | 0.2464 | 0.2503 | 0.2144 |
| $(6) > 50^{\circ}$ | 0.1693 | 0.3116 | 0.0472 | 0.4541 | 0.4384 | 0.4219 | 0.4003 | 0.4599 | 0.3289 |
| Consistency ratio: | 0.06 | 0.02 | 0.04 | 0.10 | 0.06 | 0.07 | 0.13 | 0.05 | |
| Slope aspect | | | | | | | | | |
| (1) Flat | 0.0372 | 0.0208 | 0.0271 | 0.0358 | 0.0230 | 0.0252 | 0.0340 | 0.0141 | 0.0298 |
| (2) North | 0.0432 | 0.0345 | 0.0362 | 0.0358 | 0.0317 | 0.0252 | 0.0404 | 0.1801 | 0.0386 |
| (3) Northeast | 0.2485 | 0.0695 | 0.1945 | 0.0674 | 0.0718 | 0.0566 | 0.0471 | 0.2047 | 0.1399 |
| (4) East | 0.1879 | 0.0336 | 0.0530 | 0.1678 | 0.0742 | 0.2243 | 0.0471 | 0.0996 | 0.0804 |
| (5) Southeast | 0.0849 | 0.0336 | 0.1945 | 0.0843 | 0.2001 | 0.1948 | 0.0814 | 0.0396 | 0.0986 |
| (6) South | 0.0503 | 0.2054 | 0.0530 | 0.1662 | 0.2998 | 0.0793 | 0.1263 | 0.1369 | 0.1087 |
| (7) Southwest | 0.1696 | 0.3730 | 0.1945 | 0.0843 | 0.1486 | 0.0564 | 0.2533 | 0.2293 | 0.2476 |
| (8) West | 0.1181 | 0.1960 | 0.0530 | 0.2523 | 0.0832 | 0.2762 | 0.2533 | 0.0727 | 0.1551 |
| (9) Northwest | 0.0603 | 0.0336 | 0.1945 | 0.1061 | 0.0676 | 0.0621 | 0.1172 | 0.0231 | 0.1014 |
| Consistency ratio: | 0.07 | 0.04 | 0.04 | 0.20 | 0.18 | 0.21 | 0.05 | 0.22 | |
| Slope curvature | | | | | | | | | |
| (1) Concave (-) | 0.5247 | 0.1749 | 0.2521 | 0.1285 | 0.1062 | 0.2605 | 0.4286 | 0.2605 | 0.2691 |
| (2) Flat (0) | 0.1416 | 0.0472 | 0.0726 | 0.2766 | 0.2605 | 0.1062 | 0.1429 | 0.1062 | 0.1544 |
| (3) Convex (+) | 0.3338 | 0.1113 | 0.6752 | 0.5949 | 0.6333 | 0.6333 | 0.4286 | 0.6333 | 0.4812 |
| Consistency ratio: | 0.05 | 0.10 | 0.11 | 0.00 | 0.03 | 0.03 | 0.00 | 0.03 | |
| TWI | | | | | | | | | |
| (1) < 2.5 | 0.3915 | 0.0248 | 0.0563 | 0.0469 | 0.0408 | 0.3451 | 0.0379 | 0.0249 | 0.0387 |
| (2) 2.5 - 5.0 | 0.0638 | 0.0435 | 0.4276 | 0.0677 | 0.0530 | 0.2093 | 0.0591 | 0.0439 | 0.1271 |
| (3) 5.0 – 7.5 | 0.0739 | 0.0789 | 0.3305 | 0.1132 | 0.0920 | 0.1474 | 0.1001 | 0.0956 | 0.1420 |
| (4) 7.5 – 10.0 | 0.1031 | 0.1385 | 0.0933 | 0.1132 | 0.1522 | 0.1132 | 0.1562 | 0.1574 | 0.1309 |
| (5) 10.0 – 12.5 | 0.1502 | 0.2330 | 0.0487 | 0.2140 | 0.2475 | 0.1044 | 0.2464 | 0.3904 | 0.2267 |
| (6) > 12.5 | 0.2176 | 0.4814 | 0.0436 | 0.4449 | 0.4144 | 0.0805 | 0.4003 | 0.2879 | 0.3344 |
| Consistency ratio: | 0.14 | 0.10 | 0.05 | 0.10 | 0.07 | 0.15 | 0.13 | 0.10 | |

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| Factors | CW (of each factor) from individual expert judgment | | | | | | | | Mean weight |
|---|---|------------------|------------------|--------|------------------|------------------|--------|------------------|------------------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | (CR < 0.1) |
| Drainage | | | | | | | | | |
| Distance from drainage (m) | | | | | | | | | |
| (1) < 100 | 0.3425 | 0.4625 | 0.4996 | - | 0.3598 | 0.4467 | 0.0249 | 0.3763 | 0.3408 |
| (2) 100 - 200 | 0.2067 | 0.2550 | 0.2944 | - | 0.2154 | 0.1893 | 0.0439 | 0.2959 | 0.2223 |
| (3) 200 - 300 | 0.1448 | 0.1403 | 0.0872 | - | 0.1514 | 0.1408 | 0.0956 | 0.1542 | 0.1193 |
| (4) 300 – 400 | 0.1260 | 0.0736 | 0.0409 | - | 0.1013 | 0.1033 | 0.1574 | 0.1011 | 0.0932 |
| (5) 400 - 500 | 0.1003 | 0.0343 | 0.0389 | - | 0.0911 | 0.0728 | 0.3904 | 0.0455 | 0.1273 |
| (6) > 500 | 0.0798 | 0.0343 | 0.0389 | - | 0.0810 | 0.0471 | 0.2879 | 0.0270 | 0.0970 |
| Consistency ratio: | 0.17 | 0.05 | 0.06 | - | 0.2 | 0.12 | 0.10 | 0.08 | |
| Lithology | | 0100 | 0100 | | | | 0110 | 0100 | |
| (1) Thung Yai | 0.1660 | 0.0672 | 0.0977 | 0.1075 | 0.2016 | 0.1030 | - | 0.1980 | 0.1362 |
| 2) Ratburi | 0.0328 | 0.0626 | 0.0217 | 0.0742 | 0.0685 | 0.0525 | - | 0.0540 | 0.0602 |
| (3) Sediment | 0.0528 | 0.0626 | 0.0219 | 0.0433 | 0.0319 | 0.0348 | - | 0.1170 | 0.0650 |
| (4) Kaeng Krachan | 0.1185 | 0.1195 | 0.2323 | 0.1228 | 0.0905 | 0.1773 | - | 0.0785 | 0.1262 |
| 5) Igneous rocks | 0.3778 | 0.4019 | 0.4135 | 0.2267 | 0.3622 | 0.3383 | _ | 0.3614 | 0.3088 |
| (6) Krabi | 0.1309 | 0.2241 | 0.0828 | 0.2128 | 0.0959 | 0.1919 | - | 0.0217 | 0.1421 |
| (7) Saibon Formation | 0.1309 | 0.0620 | 0.1300 | 0.2128 | 0.1494 | 0.1919 | - | 0.0217 | 0.1421 |
| Consistency ratio: | 0.1102 | 0.0020 | 0.1300 | 0.2120 | 0.14)4 | 0.1025 | - | 0.1094 | 0.1015 |
| Lineament | 0.20 | 0.20 | 0.17 | 0.02 | 0.12 | 0.02 | | 0.00 | |
| Distance from lineament (m) | | | | | | | | | |
| (1) < 500 | 0.3231 | 0.3176 | 0.5302 | 0.1692 | 0.2952 | 0.3817 | 0.4007 | 0.3515 | 0.3455 |
| (2) 500 - 1,000 | 0.2482 | 0.3176 | 0.1864 | 0.2429 | 0.1897 | 0.2486 | 0.1772 | 0.2367 | 0.2467 |
| (3) 1,000 - 1,500 | 0.2482 | 0.3170 | 0.1304 | 0.2429 | 0.1397 | 0.2480 | 0.1772 | 0.2307 | 0.2407 |
| (4) 1,500 - 2,000 | 0.1044 | 0.1073 | 0.0450 | 0.2376 | 0.1391 | 0.1349 | 0.1059 | 0.0933 | 0.1029 |
| (5) 2,000 - 2,500 | 0.1132 | 0.0944 | 0.0430 | 0.0576 | 0.1232 | 0.0800 | 0.1039 | 0.0933 | 0.0637 |
| | 0.0014 | 0.0313 | 0.0433 | 0.0576 | 0.1012 | 0.0792 | 0.0804 | 0.0893 | 0.0037 |
| $\begin{array}{c} (6) \ 2,500 - 3,000 \\ (7) > 3,000 \end{array}$ | 0.0493 | 0.0257 | 0.0475 | 0.0576 | 0.0844 | 0.0441 | 0.0387 | 0.0430 | 0.0430 |
| | 0.0382 | 0.0237 | 0.0370 | -0.02 | 0.0072 | 0.0230 | 0.0399 | 0.0200 | 0.0342 |
| Consistency ratio: Soil Texture | 0.07 | 0.04 | 0.00 | -0.02 | 0.14 | 0.02 | 0.12 | 0.07 | |
| | 0.0224 | 0.0155 | 0.0314 | 0.0783 | 0 2724 | 0.1318 | 0.0218 | 0.0174 | 0.0494 |
| 1) Clay | 0.0224 0.0722 | 0.0133 | 0.0314 | 0.0785 | 0.2734 0.3119 | 0.1318 | 0.0218 | 0.0174 0.0311 | 0.0494 |
| 2) Silty clay | 0.0722 | 0.0133 | 0.2020 | 0.0939 | 2.8293 | 0.0701 | 0.0332 | 0.0311 | 0.0743 |
| 3) Loamy sand | 0.1133 | 0.1817 | 0.0372 | 0.0511 | 2.8293 | 0.0383 | 0.1307 | 0.0873 | 0.0921 |
| (4) Sandy loam(5) Silty clay loam | | | 0.0387 | 0.0307 | 1.7464 | | 0.0491 | | |
| 6) Sand | 0.0514 0.2871 | 0.0532 0.1817 | 0.1085 | 0.0991 | 1.0172 | 0.1038 0.0262 | 0.0491 | 0.0532 0.2175 | 0.0878 0.1175 |
| | | | | | | | | | |
| 7) Sandy clay loam | 0.1125 | 0.0946 | 0.1620 | 0.0991 | 0.8624 | 0.0488 | 0.0888 | 0.0356 | 0.0882 |
| (8) Clay loam | 0.0400 | 0.0155 | 0.0344 | 0.1512 | 0.5413 | 0.1252 | 0.0483 | 0.0995 | 0.0790 |
| (9) Silty loam | 0.0779 | 0.0256 | 0.0405 0.0403 | 0.1512 | 0.4499 | 0.0772 | 0.0562 | 0.1624 | 0.0855 |
| 10) Loam | 0.0550 | 0.0532 | | 0.1512 | 0.4898 | 0.0731 | 0.0562 | 0.0831 | 0.0762 |
| 11) Slope complex area | 0.0317 | 0.1817 | 0.2135 | 0.0365 | 3.3229 | 0.2292 | 0.1833 | 0.0692 | 0.1522 |
| Consistency ratio: | 0.11 | 0.03 | 0.04 | -0.28 | 0.14 | 0.08 | 0.08 | -0.29 | |
| LULC | 0.1107 | 0.0000 | 0.2512 | 0.0771 | 0.5150 | 0.0404 | 0.0010 | 0.0224 | 0.1.420 |
| (1) Dense evergreen forest | 0.1106 | 0.0299 | 0.3512 | 0.0661 | 0.5158 | 0.0494 | 0.0912 | 0.0334 | 0.1439 |
| 2) Disturbed evergreen | 0.2052 | 0.0855 | 0.1613 | 0.2303 | 0.0858 | 0.0806 | 0.1280 | 0.0679 | 0.0896 |
| orest | 0.0000 | 0.0.000 | 0.0-10 | 0.0010 | 0.0100 | 0.4551 | 0.0-10 | 0.1540 | 0.0110 |
| 3) Oil palm | 0.2339 | 0.3600 | 0.0542 | 0.2910 | 0.2133 | 0.4561 | 0.3548 | 0.1748 | 0.3118 |
| (4) Para rubber | 0.4002 | 0.3600 | 0.1939 | 0.2773 | 0.1422 | 0.2616 | 0.3548 | 0.2508 | 0.2739 |
| (5) Miscellaneous | 0.0501 | 0.1646 | 0.2394 | 0.1352 | 0.0428 | 0.1523 | 0.0713 | 0.4731 | 0.1808 |
| Consistency ratio: | 0.11 | 0.05 | 0.14 | 0.19 | 0.09 | 0.04 | 0.08 | 0.04 | |

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Table 5 FW and class (or attribute) weights of all input factors from the AHP method in which the possible range of both weight types is from 0 (least important) to 1 (most important).

| Thematic layers | Attributes | FW | CW | FW·CW |
|-----------------|---------------------------|--------|--------|--------|
| Elevation | < 200 m | | 0.0387 | 0.0021 |
| | 200 m – 400 m | | 0.0724 | 0.0040 |
| | 400 m – 600 m | 0.0550 | 0.1165 | 0.0064 |
| | 600 m – 800 m | 0.0550 | 0.2179 | 0.0120 |
| | 800 m – 1,000 m | | 0.2298 | 0.0126 |
| | > 1,000 m | | 0.3246 | 0.0179 |
| Slope gradient | $0^{\circ} - 10^{\circ}$ | | 0.0378 | 0.0066 |
| | $10^{\circ} - 20^{\circ}$ | | 0.0733 | 0.0127 |
| | $20^{\circ} - 30^{\circ}$ | 0.1734 | 0.1459 | 0.0253 |
| | $30^{\circ} - 40^{\circ}$ | 0.1754 | 0.1997 | 0.0346 |
| | $40^{\circ} - 50^{\circ}$ | | 0.2144 | 0.0372 |
| | > 50° | | 0.3289 | 0.0570 |
| Slope aspect | Flat | | 0.0298 | 0.0015 |
| | North | | 0.0386 | 0.0020 |
| | Northeast | | 0.1399 | 0.0072 |
| | East | | 0.0804 | 0.0042 |
| | Southeast | 0.0517 | 0.0986 | 0.0051 |
| | South | | 0.1087 | 0.0056 |
| | Southwest | | 0.2746 | 0.0142 |
| | West | | 0.1551 | 0.0080 |
| | Northwest | | 0.1014 | 0.0052 |
| Slope curvature | Concave (-) | | 0.2691 | 0.0203 |
| | Flat (0) | 0.0753 | 0.1544 | 0.0116 |
| | Convex (+) | | 0.4812 | 0.0362 |
| TWI | 0 - 2.5 | | 0.0387 | 0.0031 |
| | 2.5 - 5.0 | | 0.1271 | 0.0101 |
| | 5.0 - 7.5 | 0.0794 | 0.1420 | 0.0113 |
| | 7.5 - 10.0 | 0.0771 | 0.1309 | 0.0104 |
| | 10.0 - 12.5 | | 0.2267 | 0.0180 |
| | > 12.5 | | 0.3344 | 0.0266 |
| Drainage | < 50 m | | 0.3408 | 0.0186 |
| (Distance from | 50 m – 100 m | | 0.2223 | 0.0121 |
| drainage) | 100 m – 150 m | 0.0545 | 0.1193 | 0.0065 |
| | 150 m – 200 m | 0.0515 | 0.0932 | 0.0051 |
| | 200 m – 250 m | | 0.1273 | 0.0069 |
| | > 250 m | | 0.0970 | 0.0053 |
| Lithology | Thung Yai | | 0.1362 | 0.0239 |
| | Ratburi | | 0.0602 | 0.0106 |
| | Sediment | | 0.0650 | 0.0114 |
| | Kaeng Krachan | 0.1756 | 0.1262 | 0.0222 |
| | Igneous rocks | | 0.3088 | 0.0542 |
| | Krabi | | 0.1421 | 0.0250 |
| | Saibon Formation | | 0.1615 | 0.0284 |
| Lineament | < 500 m | | 0.3455 | 0.0362 |
| (Distance from | 500 m - 1,000 m | | 0.2467 | 0.0258 |
| lineament) | 1,000 m – 1,500 m | | 0.1629 | 0.0171 |
| | 1,500 m – 2,000 m | 0.1047 | 0.1019 | 0.0107 |
| | 2,000 m – 2,500 m | | 0.0637 | 0.0067 |
| | 2,500 m – 3,000 m | | 0.0450 | 0.0047 |
| | > 3,000 m | | 0.0342 | 0.0036 |

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| Thematic layers | Attributes | FW | CW | FW·CW |
|-----------------|----------------------------|--------|--------|--------|
| Soil Texture | Clay | | 0.0493 | 0.0058 |
| | Silty clay | | 0.0743 | 0.0088 |
| | Loamy sand | | 0.0721 | 0.0085 |
| | Sandy loam | | 0.0979 | 0.0116 |
| | Silty clay loam | | 0.0878 | 0.0104 |
| | Sand | 0.1184 | 0.1175 | 0.0139 |
| | Sandy clay loam | | 0.0882 | 0.0104 |
| | Clay loam | | 0.0790 | 0.0094 |
| | Silty loam | | 0.0855 | 0.0101 |
| | Loam | | 0.0762 | 0.0090 |
| | Slope complex area | | 0.1522 | 0.0180 |
| LULC | Dense evergreen forest | | 0.1439 | 0.0161 |
| | Disturbed evergreen forest | | 0.0896 | 0.0100 |
| | Oil palm | 0.1121 | 0.3118 | 0.0350 |
| | Para rubber | | 0.2739 | 0.0307 |
| | Miscellaneous | | 0.1808 | 0.0203 |

Susceptibility map construction and validation

The susceptibility map for each examined method was built from its NSS dataset, acquired through Eqs. (1) and (2) as described earlier, and the final results are illustrated in Figures 5(a) and 5(b), respectively, in which 5 susceptibility classes were identified, from VLS to VHS. In addition, the proportion of land belonging to each classified category on these maps is described conclusively in Table 6. From these yielded products, it was found that the 2 methods produced very similar map outlooks and distributing patterns of the classified land. Both maps conclude that most parts of the land in the study area are located in the low to very low susceptibility zone (42.86 % for the WLC and 55.85 % for the AHP), while about 17.49 % (for the WLC case) and 8.79 % (for the AHP case) of the total land area were placed in the high to very high susceptibility zone (mostly along the Khao Phanom Bencha mountain network).

The capability of these maps on the prediction of actual landslide incidence occurred was assessed using 2 popular methods: the Area-Under-Curve (AUC) analysis (as detailed in [20], and the Receiver Operating Characteristic (ROC) analysis (as detailed in [21]. Reference landslide data (of 210 samples) were taken from the landslide inventory map of the area established from original landslide evidences seen in the high-resolution satellite images, as described earlier. The primary goal of the AUC method is to quantify the accurate prediction rate of the method in use, while that for the ROC curve analysis is to find a cutoff value that shall somehow minimize the number of existing false predictions (positive or negative), or maximize the sensitivity and specificity of the prediction.



Figure 5 The classified landslide susceptibility map based on (a) WLC and (b) AHP models.

| Landslide susceptibility classes | NSS | Area (%) | | |
|----------------------------------|-----------|----------|-------|--|
| | 1155 | WLC | AHP | |
| VLS | 0.0 - 0.2 | 2.11 | 7.37 | |
| LS | 0.2 - 0.4 | 40.75 | 48.48 | |
| MS | 0.4 - 0.6 | 39.66 | 35.37 | |
| HS | 0.6 - 0.8 | 16.28 | 8.03 | |
| VHS | 0.8 - 1.0 | 1.21 | 0.76 | |

Table 6 Landslide susceptibility classification of land for both examined methods.



Figure 6 Achieved accuracies of the gained susceptibility maps from both examined methods (WLC/AHP).

As reported in **Figure 6**, both tested methods performed significantly well in terms of the attained accuracy, with values greater than 80 % in both the AUC and ROC cases. However, the WLC method seemed to provide a slightly better outcome than the AHP one (about 3.39 % higher in average accuracy). Therefore, the yielded susceptibility maps from both methods were fairly accurate in predicting the occurrence of past landslide incidences seen in the area and, as such, they are very useful for the formulating of landslide prone areas maps for the purposes of the prevention and mitigation of future landslide hazards within the study area. In terms of preference, the WLC method is probably more attractive than the AHP here, regarding its higher average map accuracy, as well as the rather simple concept and straightforward working process that can be fulfilled by most available GIS software nowadays.

Conclusions

This paper reports the impressive achievement of 2 preferred analysis methods, the WLC and AHP, in producing highly accurate landslide susceptibility maps for the chosen study area (Khao Phanom Bencha Watershed in Krabi Province, southern Thailand). In both cases, the appropriate weights at factor and attribute (or class) levels were evaluated first, based on the collected judgments on this issue of 8 corresponding experts, to serve as the basis for the determination of LSS and NSS afterwards. In general, the order of merit at both factor level and attribute level (in terms of the given weight), conforms rather well to conventional beliefs or prevalent theories. For example, the most important contributing factors were found to be slope gradient, lithology, and soil texture, while areas with relatively steep slopes were rated more susceptible to slope failure, as well as those located fairly close to drainage or lineament, or over the slope-complex land, or with igneous rock foundation. For the LULC aspect, para rubber and oil palm plantations were rated the most significant causes of landslide activity within the area.

The susceptibility map for each considered method was built from its NSS dataset for the whole area, wherein 5 susceptibility classes were shown, from VLS to VHS. It was found that both map products were highly similar in terms of the general outlook and the distributing pattern of the classified area, from which most lands were found located in the low to very low susceptibility zone (42.86 % for

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the WLC and 55.85 % for the AHP) while a considerable amount of land was placed in the high to very high susceptibility zone (17.49 % for the WLC case and 8.79 % for the AHP case), mostly concentrated along the Khao Phanom Bencha mountain network. The average accuracies of the susceptibility maps achieved by both methods were prominently high, at 85.81 % (WLC) and 82.42 % (AHP), respectively, which ensure their applicability to further applications on landslide prevention and mitigation planning within the area. In this work, the WLC method was considered more preferable than the AHP method, regarding its superior performance in map production, along with the rather simple concept and direct working process.

Notably high accuracy of the yielded susceptibility maps in both cases indicate that the accumulated expert knowledge used in this work was fairly effective in the preparation of the landslide susceptibility map for the study area. It also highlights great concern on rather fragile geologic structure over an area, and the negative impact of the oil palm and para rubber planting on increasing potential landslide activity in the area. However, as both used methods (WLC and AHP) are of a qualitative type, whose decisions rely mainly on expert opinion, in terms of knowledge enhancement, some famous quantitative type methods, which base their judgement on actual landslide data (e.g., FR or MLR) should be applied to find the most appropriate landslide susceptibility mapping method for the area as well (apart from those reported here).

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